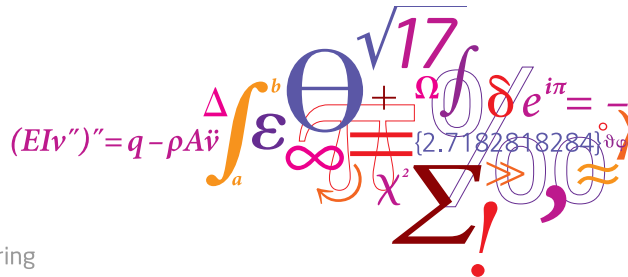
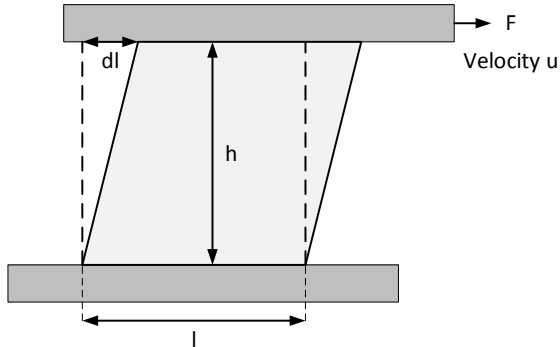


# Viscosity measurement at high pressures

Peter Christiansen



# What is viscosity?



$$\gamma = \frac{dl}{h} = \frac{u dt}{h}$$

$$\dot{\gamma} = \frac{d}{dt} (\gamma) = \frac{u}{h}$$

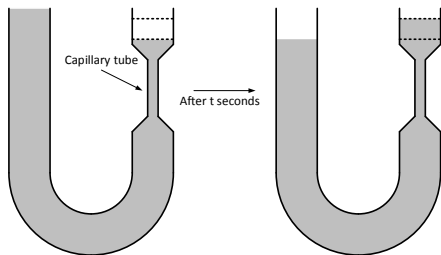
$$\tau = \eta \dot{\gamma}$$

Relationship between shear strain rate  $\dot{\gamma}$  and shear stress  $\tau$

$\eta$  is typically a function of both shear rate, pressure, temperature and fluid chemistry

# Viscosity measurement

## Capillary viscometer



$$\eta = k\rho t$$

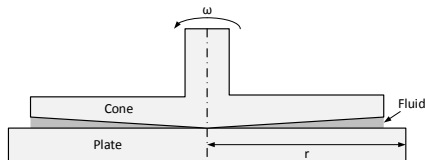
$k$  is the capillary constant measured by a reference liquid

$\rho$  is the density of the fluid

Temperature can be varied but not pressure or shear rate

# Viscosity measurement

## Cone on plate viscometer



$$\eta = kM/\omega$$

$k$  is the viscometer constant measured by a reference liquid

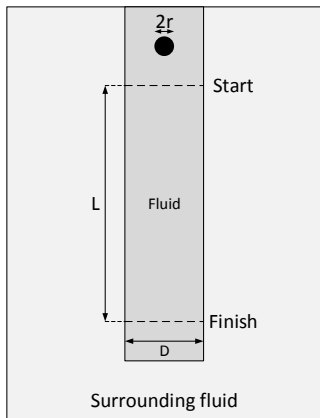
$M$  is shear torque

$\omega$  is the angular velocity

Temperature and shear rate can be varied but not pressure

# Viscosity measurement

## Falling ball viscometer



$$\eta = 2r^2 (\rho_s - \rho_f) g F / 9u$$

$g$  is the gravitational constant

$u$  is the velocity of the sphere

$\rho_s$  is the density of the sphere

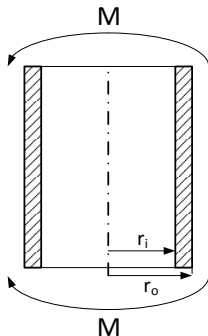
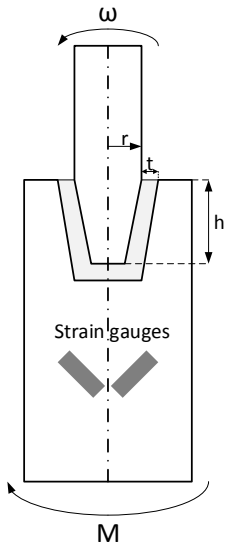
$\rho_f$  is the density of the fluid

$$F = 1 - 2.104 (d/D) + 2.09 (d/D)^3 - 0.9 (d/D)^5$$

$$d = 2r$$

Temperature and pressure can be varied but not shear rate

# New viscometer concept



$$u = r\omega$$

$$\dot{\gamma} = \frac{u}{t}$$

$$\tau = \eta\dot{\gamma}$$

$$M = \tau A (r + t) = \frac{\eta\omega 2\pi r h}{t} (r + t)^2$$

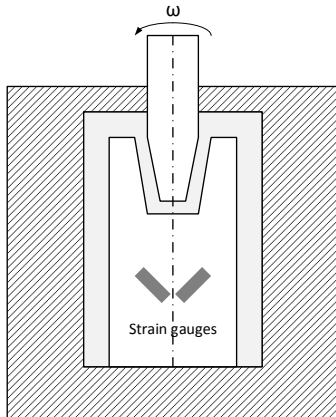
If  $t \ll r$

$$M \approx \frac{2\pi\eta\omega h r^3}{t}$$

$$\tau_{max} = \frac{2Mr_o}{\pi(r_o^4 - r_i^4)}$$

Temperature and shear rate can be varied but not pressure

# New viscometer concept



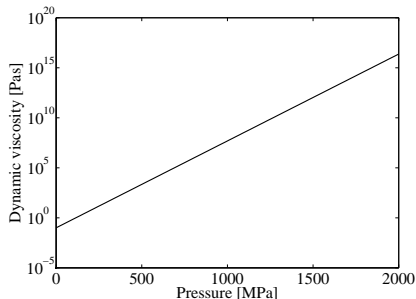
- Dimensions?
- Torque?
- Material?

Temperature, shear rate and pressure can be varied

# Torque estimation based on Barus equation

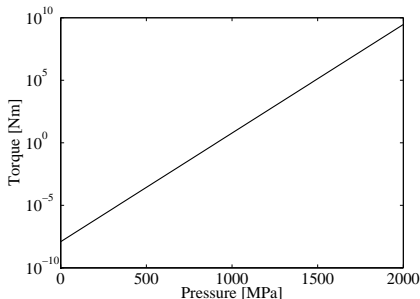
Barus equation:  $\eta = \eta_o e^{\alpha P}$

$\eta_o \approx 0.1 \text{ Pas}$ ,  $\alpha \approx 20 \cdot 10^{-9} \text{ m}^2/\text{N}$



$M \approx 2r^2\pi h\eta\frac{\omega}{t}$

$r = 5\text{mm}$ ,  $h = 25\text{mm}$ ,  $t = 1\text{mm}$ ,  $\omega = 2\pi/s$



Possibility to encounter differences in torque during experiments.

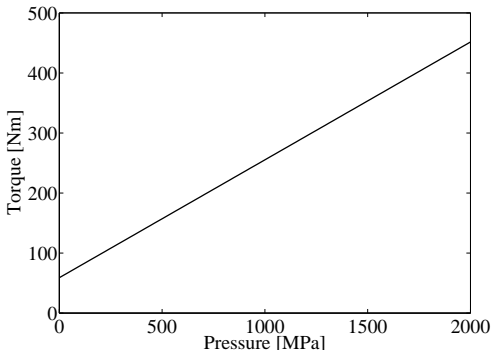


# Torque estimation based on maximum shear strength of oil

$$\tau_L = \tau_o + ap \quad M \approx 2\pi hr^2 \tau_L$$

$$\tau_o \approx 15 \text{MPa}$$

$$a \approx 0.05$$



Dimensioning torque: 40NM. Number with some uncertainty.

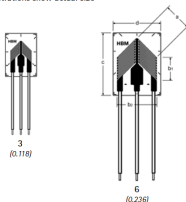
# Design of strain gauge setup

## Strain gauge from HBM

### K-XY4x

Shear/torsion half bridge  
 Temperature response matched to customer's choice  
 see page 16

Illustrations show actual size



Contents per package: 5 pcs.

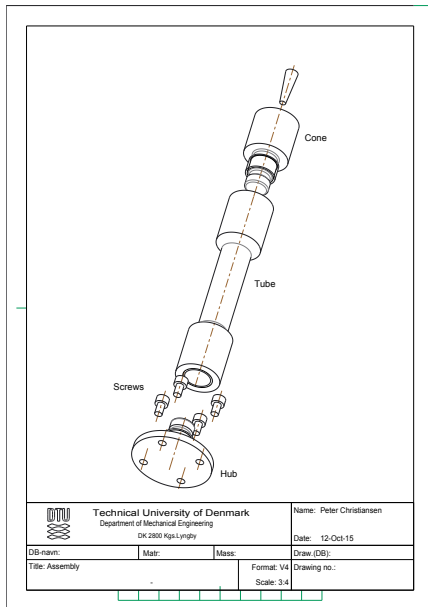
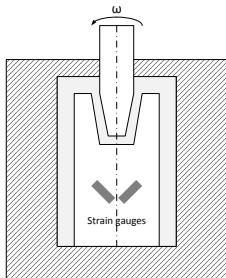
Types available at short notice		Variants <sup>(1)</sup>	Nominal resistance	Dimensions (mm/inch)					Max. perm. effective bridge ex. voltage	Solder terminals
Steel	Aluminum			Other	Measuring grid			Measuring grid carrier		
			$\Omega$	a	b1	b2	c	d	V	not required
		K-XY4x-3/120	120	3 0.118	3 0.12	5.4 0.21	11 0.433	8 0.315	5	
		K-XY4x-6/120	120	6 0.236	6 0.24	10.2 0.40	16 0.630	12.2 0.480	9.5	
		K-XY4x-3/350	350	3 0.118	4.2 0.17	5.6 0.22	11 0.433	8 0.315	9.5	
		K-XY4x-6/350	350	6 0.236	6 0.24	10 0.39	16 0.630	12.2 0.480	16	
		K-XY4x-3/700	700	3 0.118	4.2 0.17	5.6 0.22	11 0.433	8 0.315	13.5	
		K-XY4x-6/700	700	6 0.236	6 0.24	10 0.39	16 0.630	12.2 0.480	23	

<sup>(1)</sup> Variants: Minimum order quantity: 3 packages

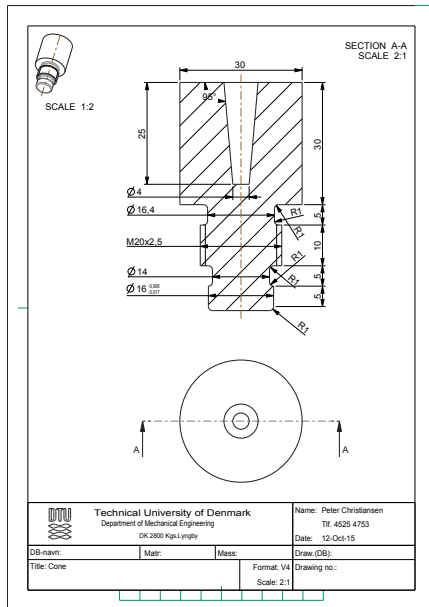
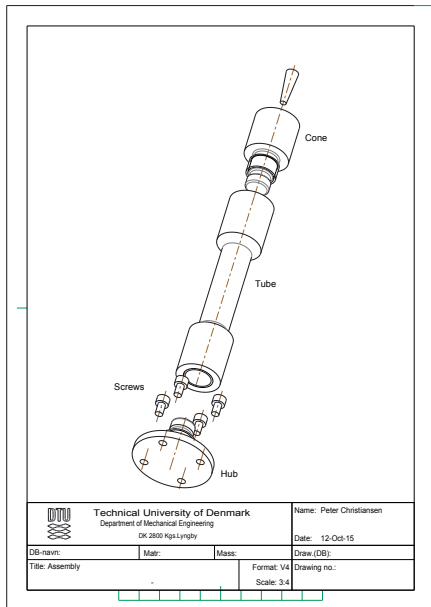
<sup>(4)</sup> Types are only available with matching to aluminum, ferritic or austenitic steel

Strains < 0.001 and uniform

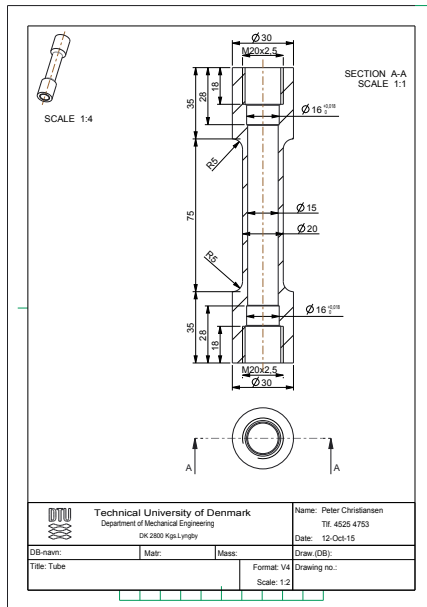
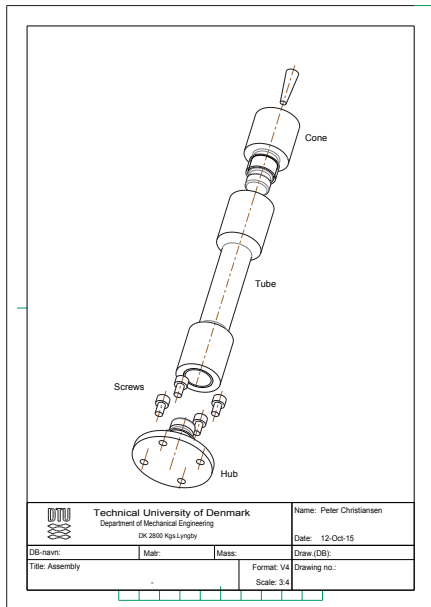
# Design of strain gauge setup



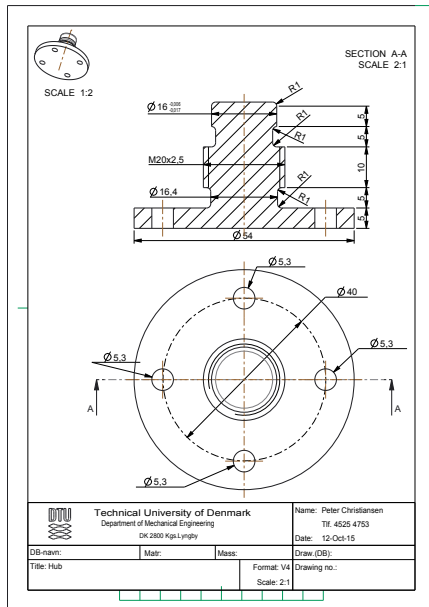
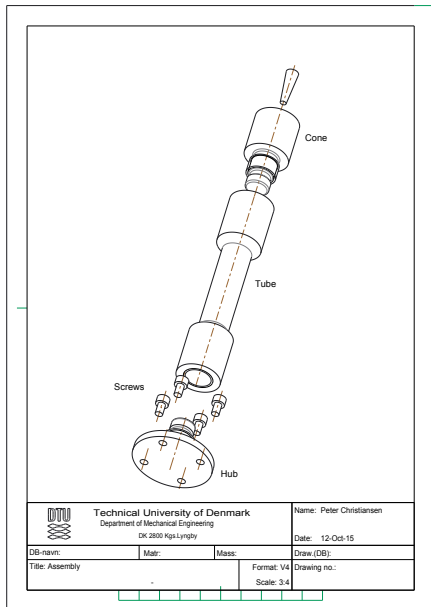
# Design of strain gauge setup



# Design of strain gauge setup

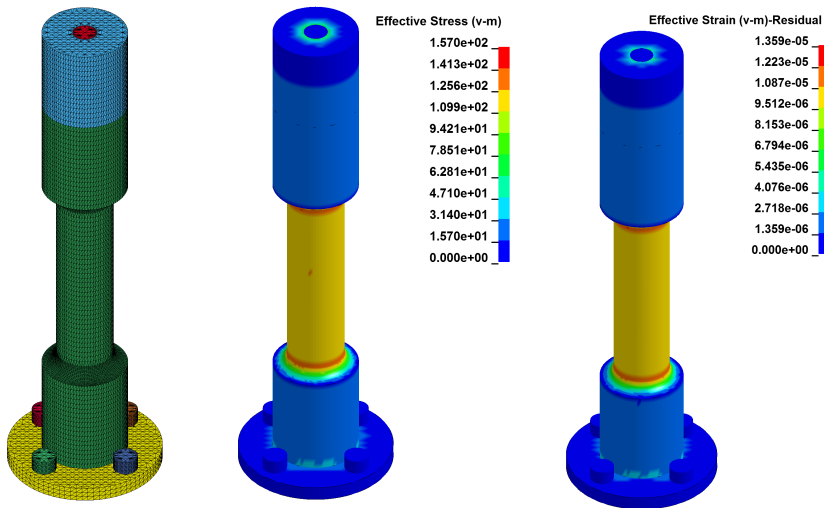


# Design of strain gauge setup



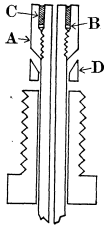
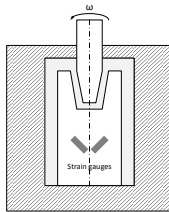
# Design of strain gauge setup

LS-DYNA simulation

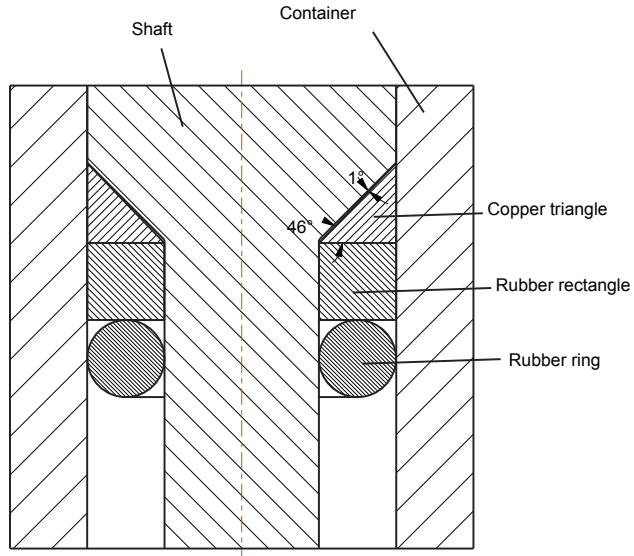


# Sealing between shaft and chamber

Bridgman seal.  $44^\circ$  or  $46^\circ$ ?



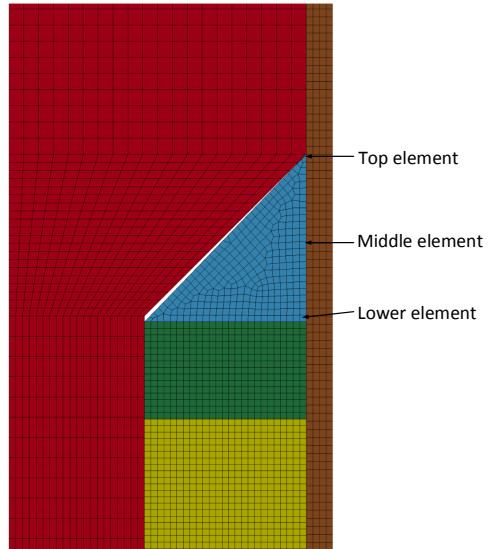
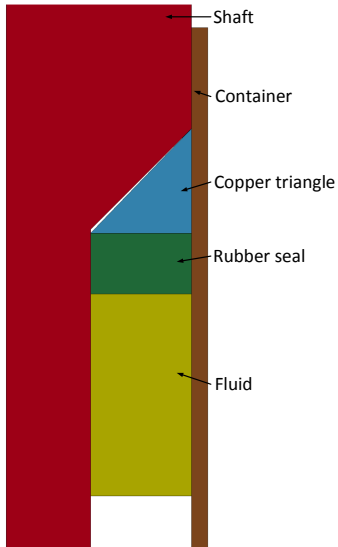
Bridgman (1914)



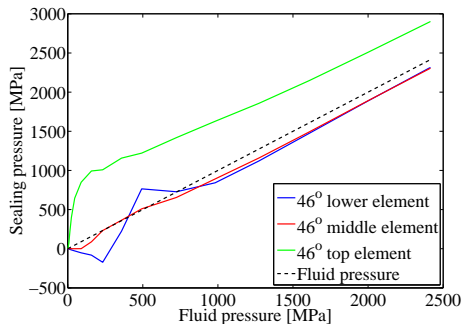
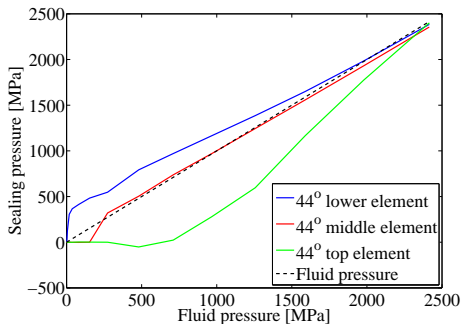


# Bridgman seal

LS-DYNA simulation



# Bridgman seal



46° gives larger closure pressure

## Possible material for construction

Uddeholm suggests to immerse possible tool steel candidates for construction into relevant oils for corrosion testing.

Sverker 21 after immersion into TDN81 (chlorinated paraffin oil) for 14 days.



# Future challenges

- Chamber pressurization
- Wires from data acquisition inside chamber to outside

Questions?