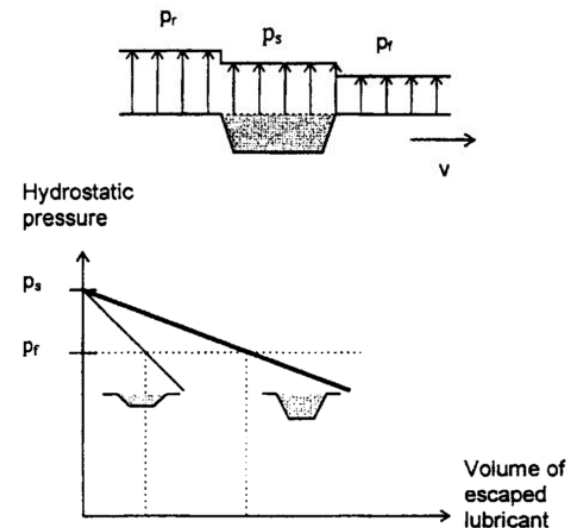
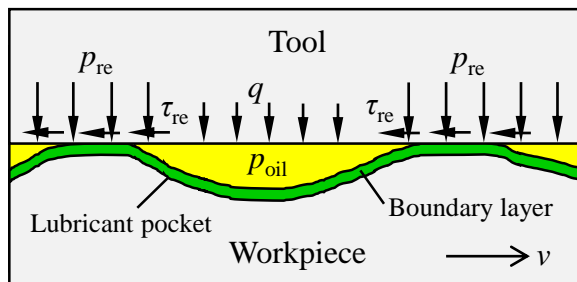




# Introduction

- When the pressure between surfaces increases, a confined lubricant in closed pockets will be a factor determining possible hydrodynamic and hydrostatic lubrication mechanism.
- How is the lubricant carry the load at different pressures?
- Are there any differences between a lubricant with and without boundary lubrication as the oil pressure increases in the pockets?
- Increased knowledge about the lubricant compressibility is required in order to design tailored surfaces for metal forming.



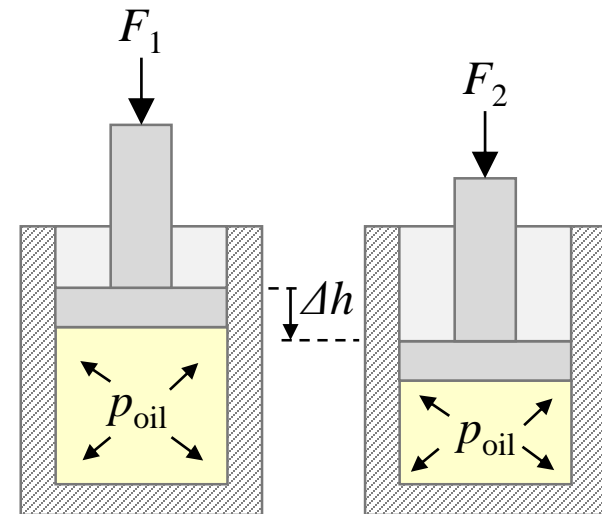
# Introduction

- Bulk modulus is a property that measures the compressibility of a fluid.

- Bulk modulus

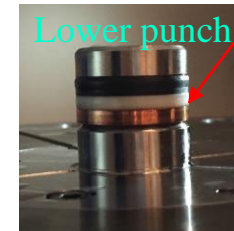
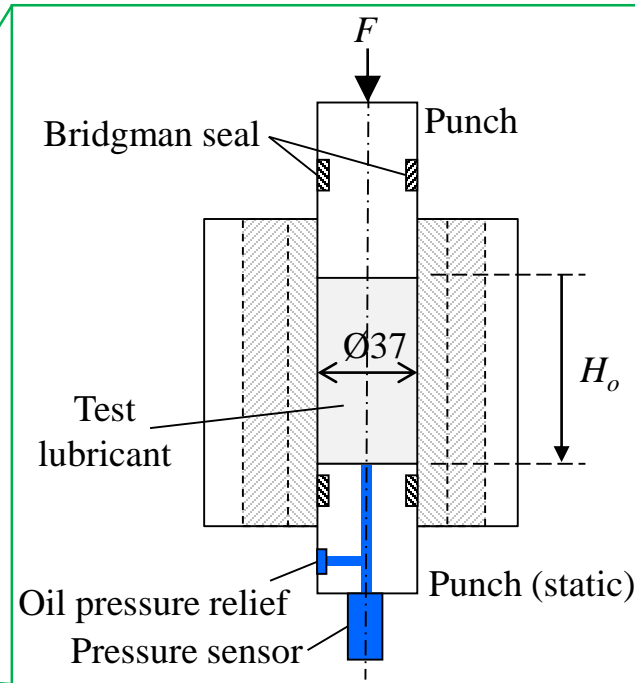
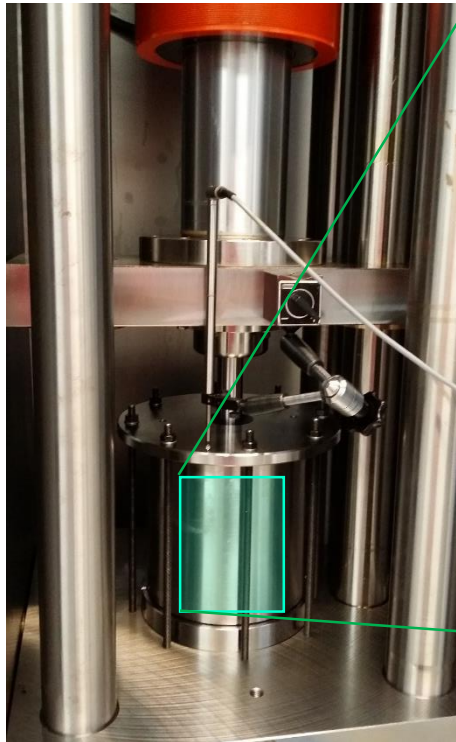
- The product of fluid volume at any specified pressure.

$$K_t = -V \frac{dP}{dV}$$

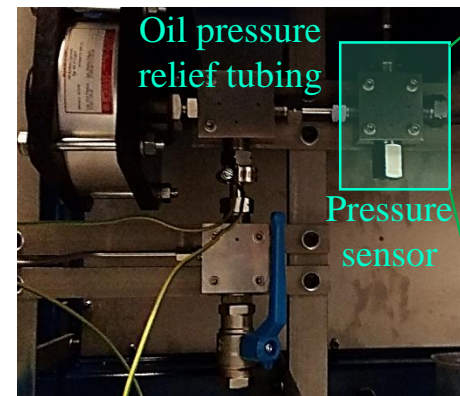


# High Pressure Equipment

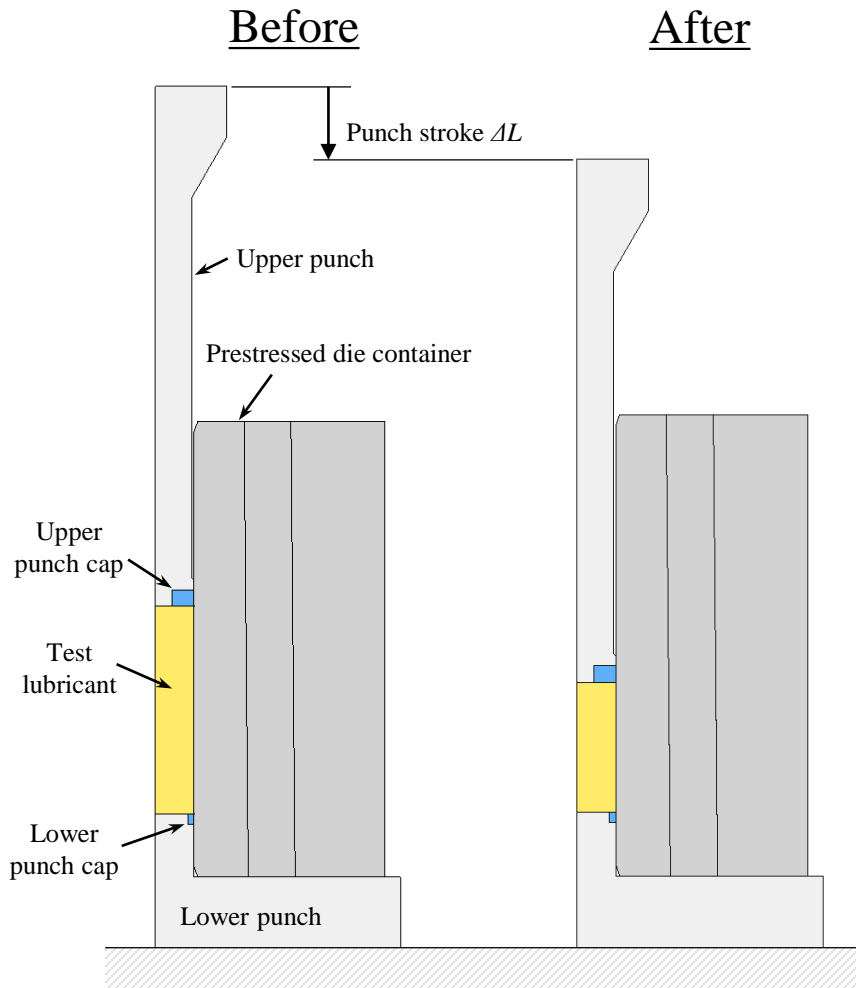
- Built-in high pressure equipment at DTU-MEK.



- Bridgman seal (<500MPa):
- Copper (Brown)
  - Teflon (White)
  - Trelleborg (Black)



# Pressure limit check (by Numerical simulation)

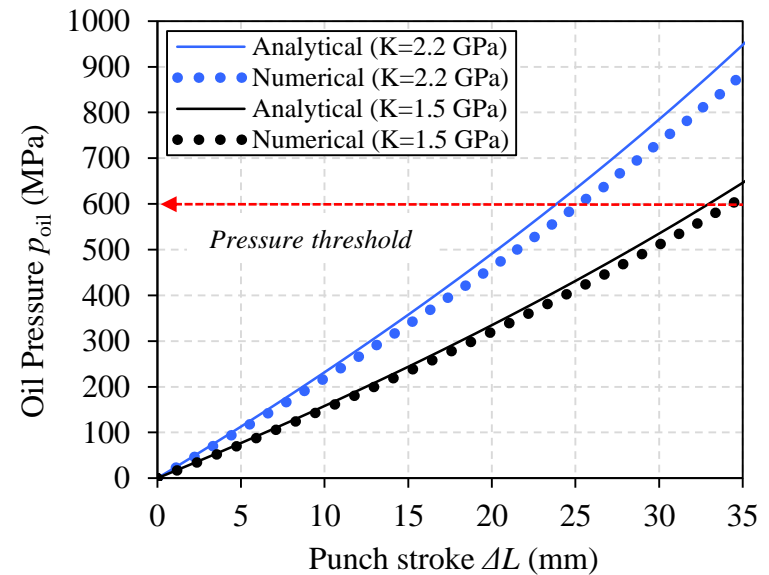


## Material properties:

- Punches: Unimax,  $E = 213$  GPa.
- Punch cap: AISI 316,  $E = 193$  GPa.
- Prestressed die container: Vanadis 4E,  $E = 206$  GPa

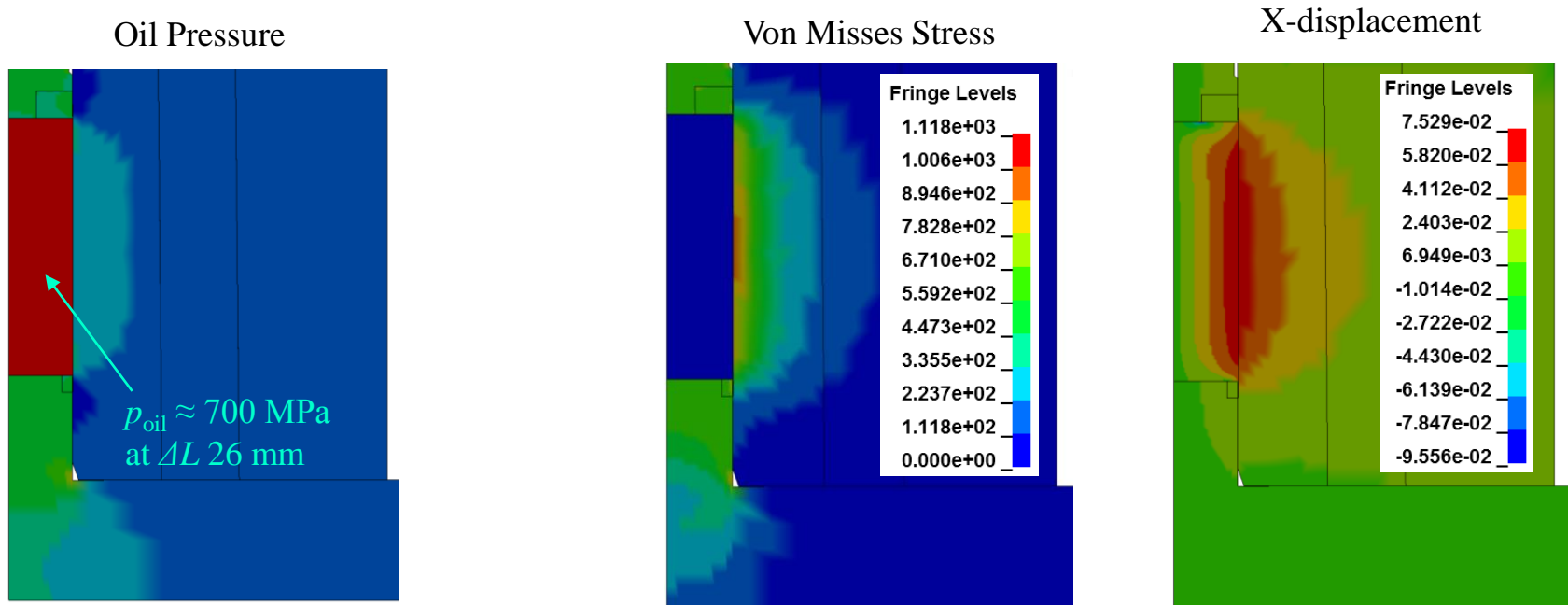
## Lubricant properties:

- Bulk modulus:
  - $K = 1500$  MPa.
  - $K = 2200$  MPa.

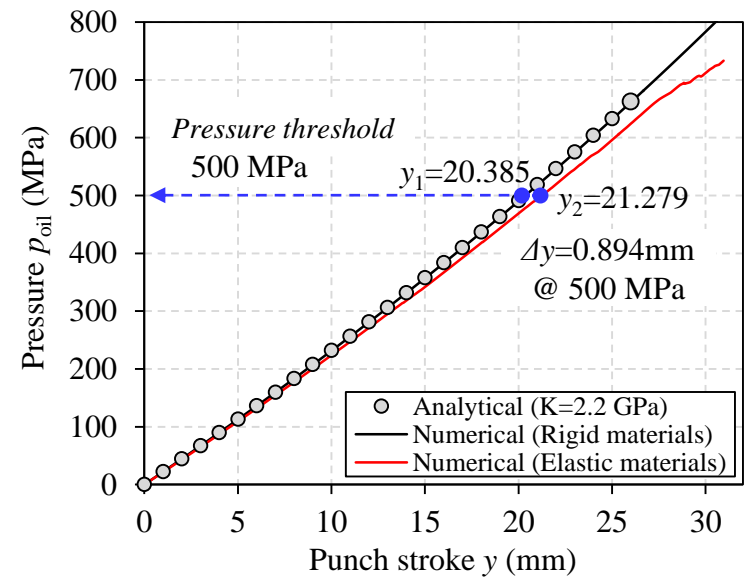
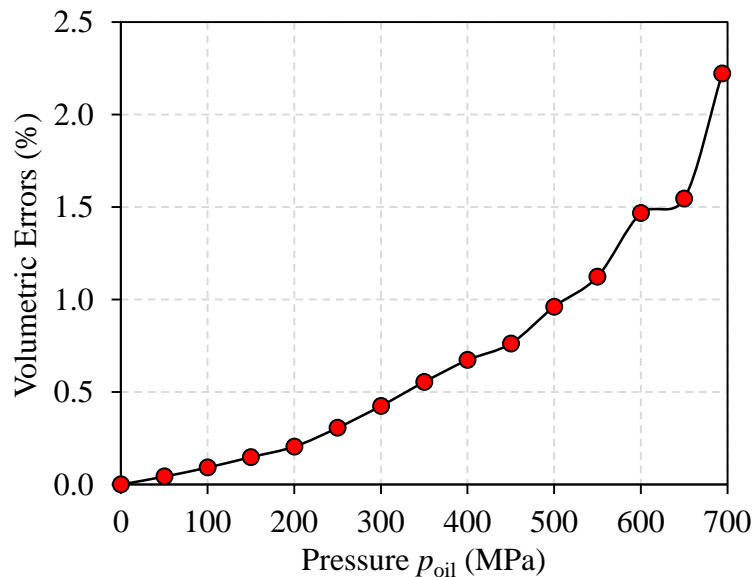
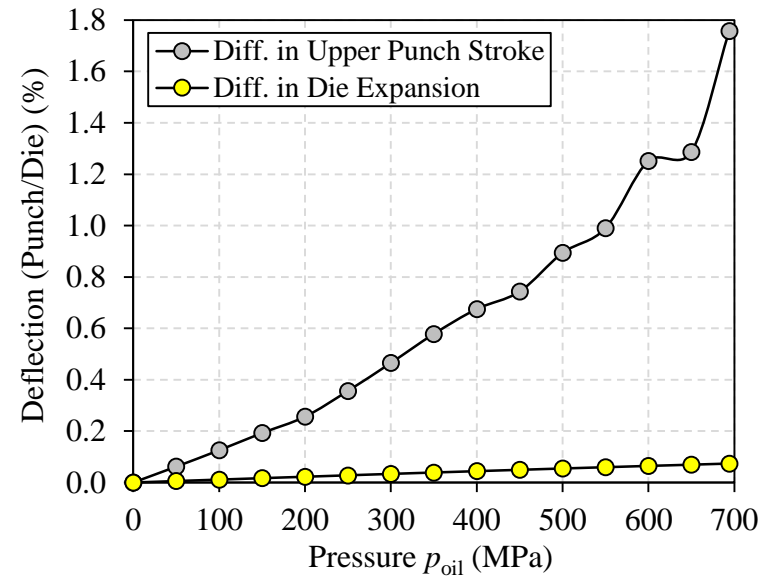
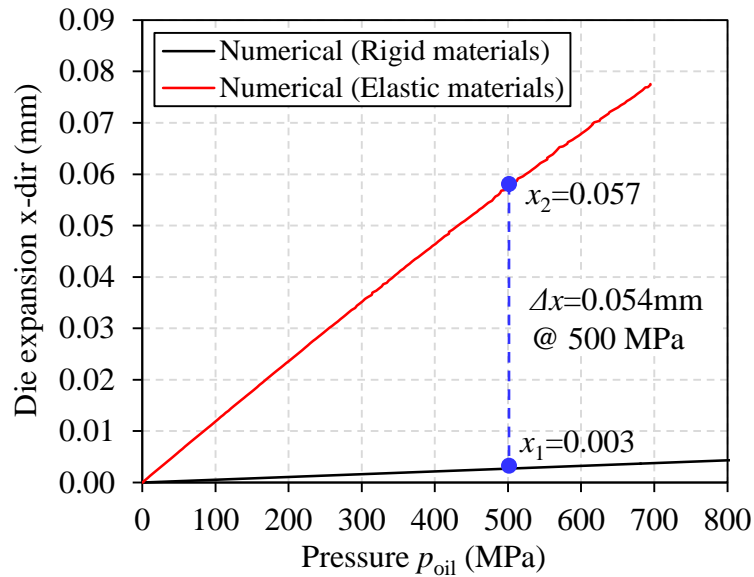


# Pressure limit check (by Numerical simulation)

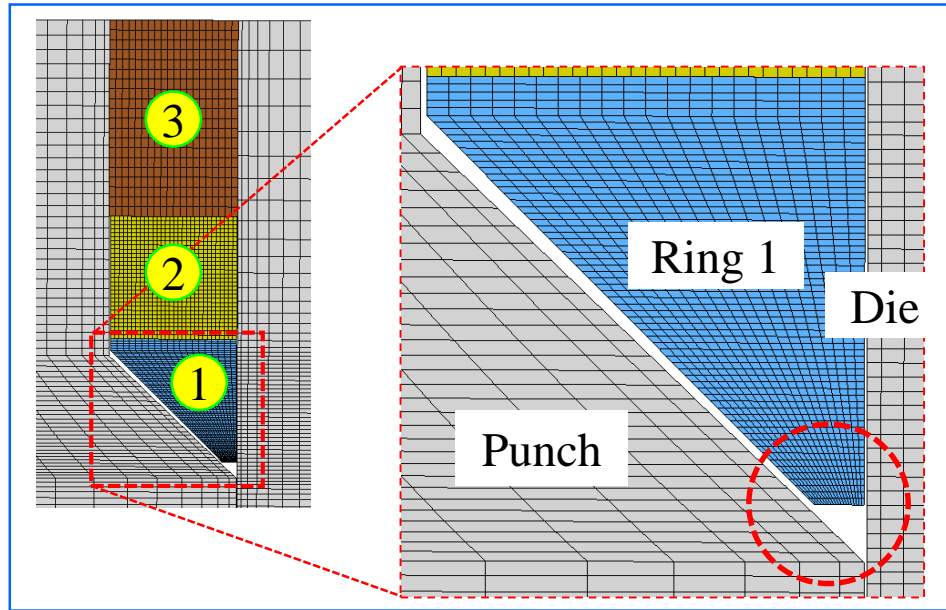
- No marked expansion on the die and the punches.



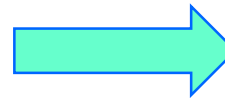
# Pressure limit check (by Numerical simulation)



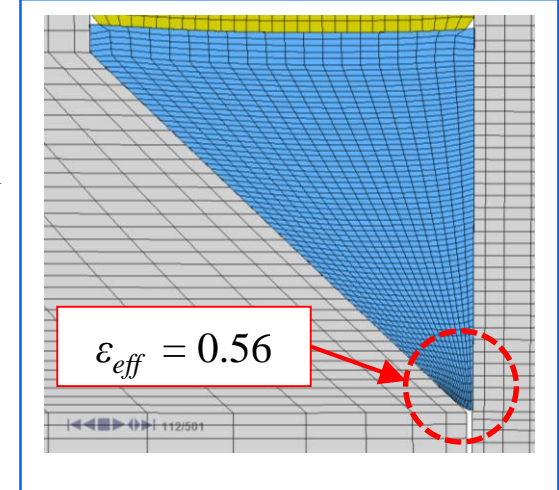
# Bridgman seal check (by Numerical simulation)



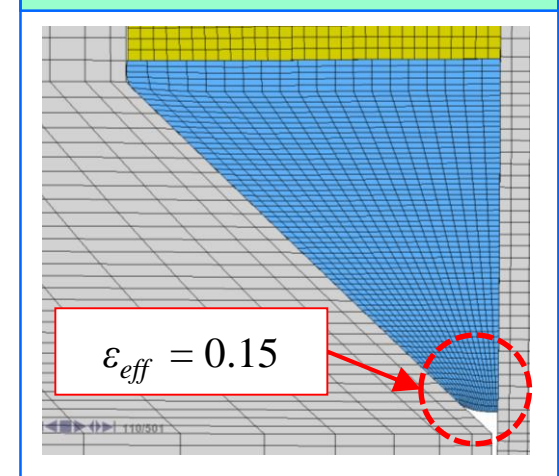
Pressing ring 3 down to 0.5mm



Ring 1 (Copper)



Ring 1 (Stainless steel)

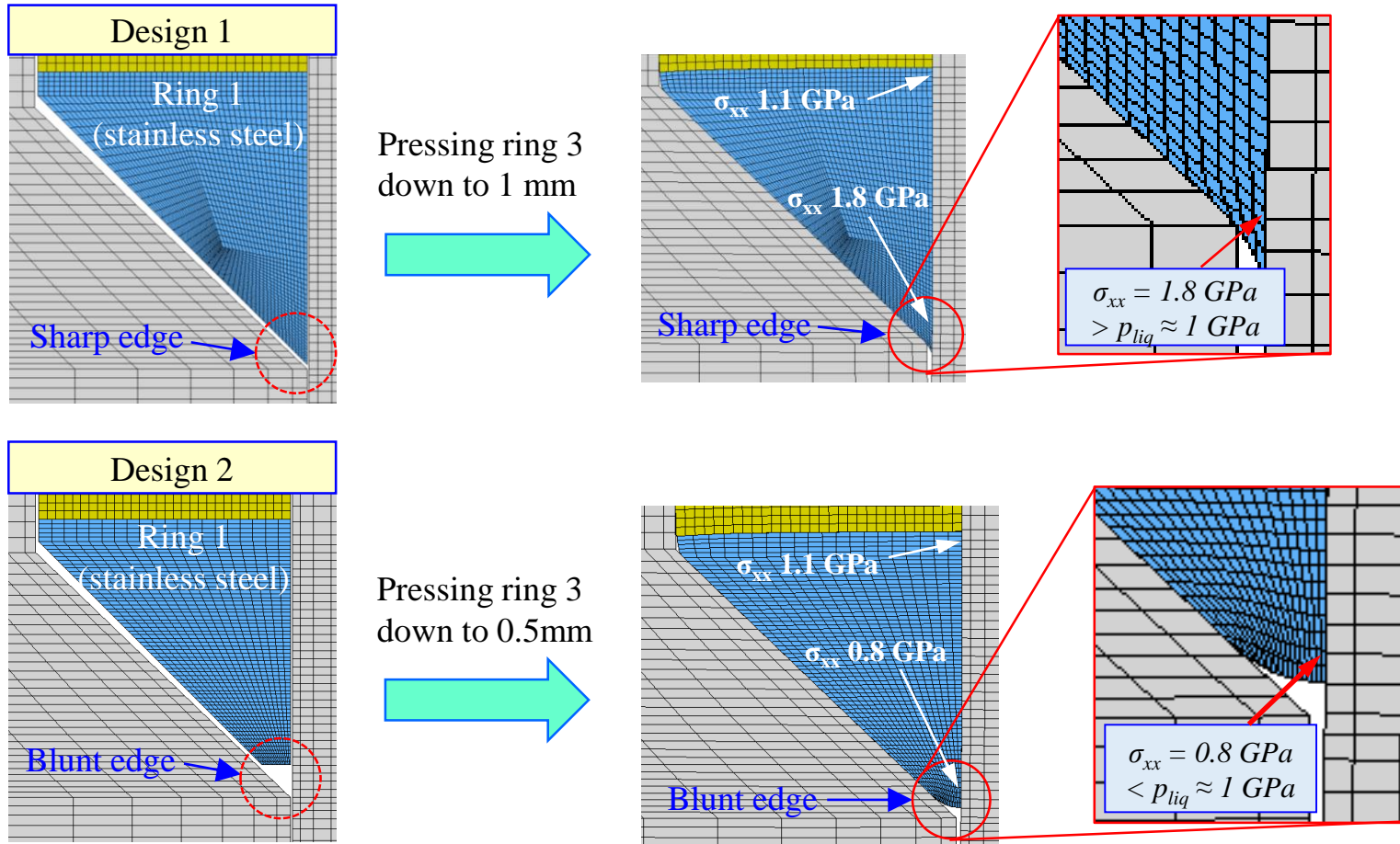


Part	Material	Mechanical Properties
Punch	Unimax	$E = 216 \text{ GPa}$
Die	Vanadis 4E	$E = 206 \text{ GPa}$
Ring 1	Copper, or Stainless steel 304	$\sigma_o = 315 \cdot \epsilon^{0.54}$ $\sigma_o = 1275 \cdot \epsilon^{0.45}$
Ring 2	Steel Ma8	$\sigma_o = 636 \cdot \epsilon^{0.23}$
Ring 3	Stainless steel 304	$\sigma_o = 1275 \cdot \epsilon^{0.45}$



# Bridgman seal check (by Numerical simulation)

- Modified design of ring 1



# Test Lubricants

- There are 3 types:
  - 1) Water (for verification with the published data).
  - 2) Plain mineral oils (Thick and thin version).
  - 3) Good boundary lubricants (Thick and thin version).

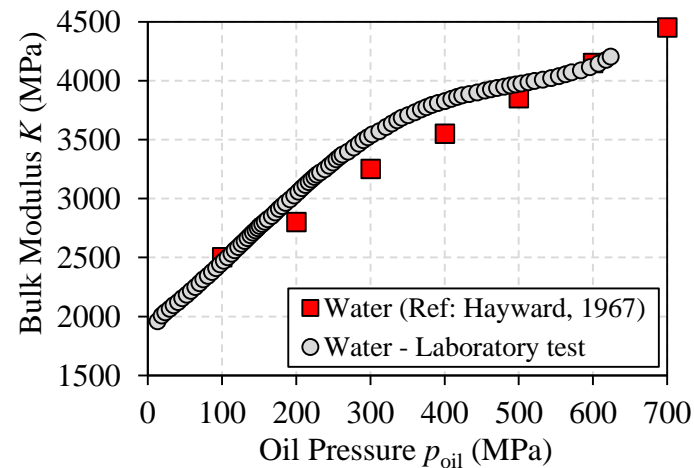
Oil type	Product name	Kinematic Viscosity $\eta_V$ @ 40°C [cSt]
-	Water	0.658
Naphthenic plain mineral oil	CR5	660
Plain mineral oil*	CR5-Sun 60	60
Mineral oil with additives	Rhenus LA 722086	800
Mineral oil with additives	Rhenus LA 722083	300
Chlorinated paraffin oil	TDN81	150

\*50 wt. % mixture oil – Houghton Plunger CR5 ( $\eta=660$  cSt) and Sunoco Sun 60 ( $\eta=10$  cSt).

# Results

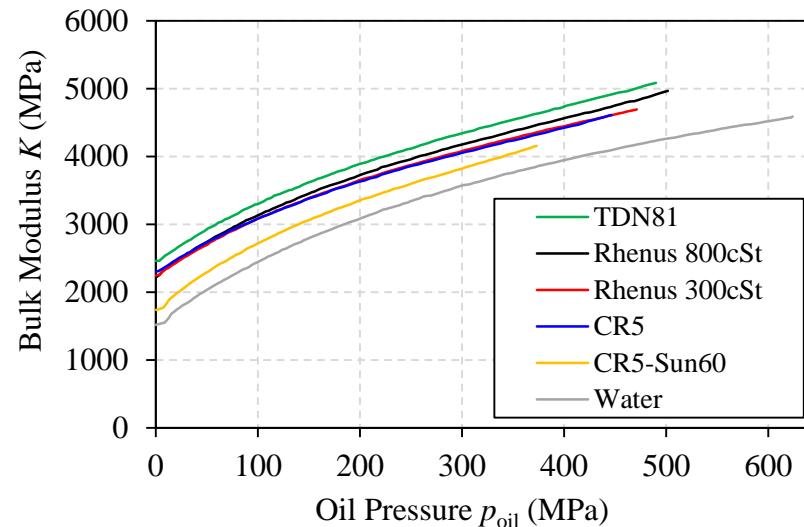
Verification of the built-in equipment at DTU-MEK

- Bulk modulus of water was compared with the established result.



# Results

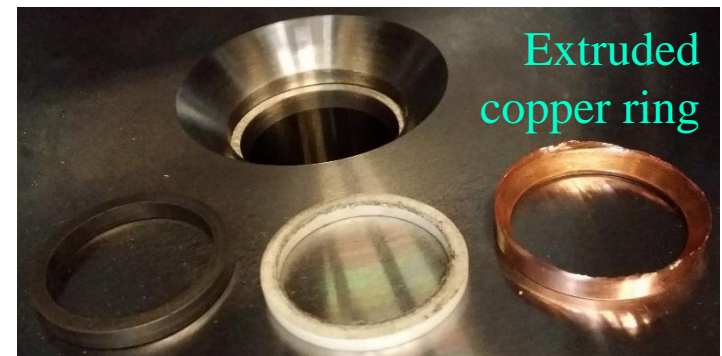
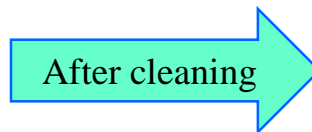
- Bulk modulus at different pressures.



- The boundary lubricants has a marked influence on compressibility when compared to the thin plain mineral oil.
- Meanwhile, the thick plain mineral oil shown a good compressibility in comparison to that of the boundary lubricant (medium viscous version).

# Results

- A light damage on the seals caused by testing of plain mineral oil (a thin oil version).

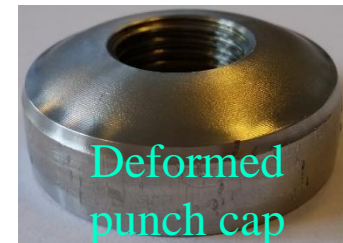


# Results

- Heavy damage on the punch cap and the seals caused by testing of plain mineral oil (a thick oil version).



After cleaning



# Summary

- The compressibility test results shown a similar trend when evaluating the same oil types on textured tool surfaces in strip reduction testing.
- The compressibility of the lubricant may be an influential factor in determining possible hydrodynamic and hydrostatic lubrication mechanism.
- The influence of the lubricant compressibility need to take into account for a future work in modelling trapped lubricant behavior in metal forming operation.